

ARTICLE

Calculation of the different shielding properties of locally developed ilmenite-magnetite (I-M) concrete

Hossain Sahadath¹, Abdus Sattar Mollah², Khorshed Ahmad Kabir¹ and Md. Fazlul Huq^{1,*}

¹ Department of Nuclear Engineering, University of Dhaka Dhaka-1000, Bangladesh.

² Bangladesh Atomic Energy Commission, Bangladesh.

Received 28 November 2014 – Accepted 5 February 2015

Abstract – In this study the total atomic cross-section (σ_a), total electronic cross-section (σ_e), effective atomic number (Z_{eff}) and effective electron density (N_{eff}) of locally developed ilmenite-magnetite (I-M) concrete were calculated analytically for different photon energies from 1 keV to 20 MeV and compared with concretes of different densities and compositions. The effect of Z_{eff} on the mass attenuation coefficient (μ/ρ , σ_a , σ_e) is shown graphically. The values of σ_a , σ_e , Z_{eff} and N_{eff} of I-M concrete were found to be higher than those of the ordinary concretes and in some cases than those of heavy concretes, which proved I-M concrete's shielding effectiveness. The results of this study will provide some useful information for a shielding material database for practical shielding calculation.

Keywords: atomic cross-section / electronic cross-section / effective atomic number / effective electron density

1 Introduction

To enable personnel to work in the vicinity of a nuclear installation, it is necessary to attenuate the radiation in a biological shield surrounding the radiation sources, so as to reduce the radiation dose to a tolerable level in the region beyond the shield. This is usually achieved by surrounding the radiation source with a sufficiently large mass of high-density material. Concrete is inexpensive and has structural strength as well as good shielding characteristics. In view of these advantages, concrete has been widely used as a shielding material. The most commonly used types of concretes are those based on barite, serpentine, steel magnetite, ordinary concrete, etc. The heavy concretes have proved themselves to be the most suitable materials for the attenuation of gamma radiation. At the beach sand processing plant in Cox's Bazar, in Bangladesh, ilmenite and magnetite sand are obtained in huge quantity as tailings. Investigation showed that these materials have great potential in the development of high-density concrete to be used as a shield. The ilmenite-magnetite (I-M) concrete is a heavy concrete produced locally with sand, stone chips and cement in the ratio 100:100:36 by volume, respectively. It has been used as the shield of the 3MW (Thermal) TRIGA Mark II Research Reactor at the Atomic Energy Research Establishment in Bangladesh. The gradation and composition of its aggregates are shown in Table 1 and the elemental composition is shown in Table 2. The knowledge of parameters such as the total atomic cross-section (σ_a), total electronic cross-section (σ_e), effective atomic number (Z_{eff}) and effective electronic

Table 1. I-M concrete aggregates.

Coarse aggregate [stone chip gradation (vol%)]	
	3.81 cm down - 20 black (crusher)
	2.54 cm down - 30 black (crusher)
	1.91 cm down - 35 black (crusher)
	1.27 cm down - 15 black (crusher)
Fine aggregate composition (vol%)	
Ordinary sand	20
Ilmenite	40
Magnetite	40
Mix ratio (cement:sand:stone chips)	36:100:100
Net water /cement ratio	0.5
Slump (cm)	1.27

density (N_{eff}) plays an important role in understanding the physical properties of any concrete. Scattering and absorption of X-ray and gamma radiation are related to the density and atomic number of an element. In composite materials, they are related to the effective atomic number and effective electron density.

Many experimental and theoretical studies have been performed on the total atomic cross-section, total electronic cross-section, effective atomic number and effective electronic density of different materials for different photon energies such as Au alloys (Han and Demir, 2010), Ti and Ni alloys (Han and Demir, 2009), carbon steel and stainless steels (Singh and Badiger, 2013), steel types 304 and 347 (Al-Jaff, 2013), polymers (Kucuk *et al.*, 2013), alkali halides (Madhusudhan Rao *et al.*, 2013), solid-state track detectors (Medhat, 2011),

* Correspondence: fazlul.huq@du.ac.bd

Table 2. Elemental composition of I-M concrete.

Element	Atomic number	Atomic mass (g)	Elemental density (g cm ⁻³)	Weight fraction	Total density (g cm ⁻³)
H	1	1.008	0.0157	0.005647	
C	6	12.011	0.0022	0.000791	
O	8	16.000	1.0523	0.378525	
Mg	12	24.320	0.1014	0.036474	
Al	13	26.980	0.0497	0.017877	
Si	14	28.090	0.1349	0.048525	
P	15	30.975	0.0002	0.000071	
S	16	32.066	0.0016	0.000575	2.78
Ca	20	40.080	0.2469	0.088812	
Ti	22	47.900	0.3563	0.128165	
V	23	50.950	0.0021	0.000755	
Cr	24	52.010	0.0010	0.000359	
Mn	25	54.940	0.0084	0.003021	
Fe	26	55.850	0.7863	0.282841	
Ni	28	58.710	0.0012	0.000431	

Table 3. Comparison of the half-value layer (HVL) of different concretes.

Photon energy (MeV)	Half-value layer (atom cm ⁻²)				
	I-M	Ordinary-1	Ordinary-2	Barite	Serpentine
6.000	0.415	0.720	0.656	0.154	0.776
8.000	0.436	0.790	0.714	0.149	0.851
10.000	0.443	0.834	0.750	0.143	0.900
12.000	0.443	0.856	0.766	0.138	0.924
15.000	0.443	0.890	0.791	0.130	0.961
18.000	0.437	0.900	0.797	0.125	0.973
20.000	0.433	0.907	0.800	0.121	0.980

concrete materials (Yilmaz *et al.*, 2011; El-Khayatt and Akkurt, 2013), etc. There have been some experimental and theoretical investigations to determine the neutron-shielding properties of I-M (Bhuiyan *et al.*, 1991; Ahmed *et al.*, 1992, 1999). There are almost no reports on the study of σ_a , σ_e , Z_{eff} and N_{eff} of this locally developed concrete for different photon energies. This prompted us to carry out this work. The objective of this study is to generate a database for σ_a , σ_e , Z_{eff} and N_{eff} of this locally developed concrete, which will be helpful for practical shielding calculation.

2 Theoretical background and calculation

2.1 Total atomic cross-section (σ_a) and electronic cross-section (σ_e)

The atomic attenuation coefficient (σ_a) is the fraction of an incident gamma-ray beam that is attenuated by a single atom. Another way of saying the same thing is that the atomic attenuation coefficient is the probability that an absorber atom will interact with one of the photons in the beam. Note that the dimensions of σ_a are cm², the units of area. For this reason, the atomic attenuation coefficient is almost always referred to as the cross-section of the absorber. The unit in which the cross-section is specified is the barn, b.

The electronic attenuation coefficient is the fraction of an incident gamma-ray beam that is attenuated by a single

electron. The electronic attenuation coefficient is also called the electronic cross-section and is symbolized by σ_e . The total atomic cross-section σ_a and the total electronic cross-section σ_e can be obtained by the following formulas:

$$\sigma_a = \frac{1}{N_A} \sum_i f_i A_i \left(\frac{\mu}{\rho} \right)_i \quad (1)$$

$$\sigma_e = \frac{1}{N_A} \sum_i f_i \frac{A_i}{Z_i} \left(\frac{\mu}{\rho} \right)_i \quad (2)$$

where f_i is the fractional abundance of element i in the mixture; $Z_i A_i$ are the atomic number and atomic mass, respectively, $\left(\frac{\mu}{\rho} \right)_i$ is the total mass attenuation coefficient of the i th element in the mixture and N_A is Avogadro's number.

2.2 The effective atomic number (Z_{eff}) and effective electron density (N_{eff})

The effective atomic number of a material is the atomic number of a hypothetical element that attenuates photons at the same rate as the material. In composite material, a single number cannot represent the atomic number uniquely across the entire energy range, as the partial interaction cross-sections have different atomic number dependence. The effective atomic

numbers of the concrete samples were obtained by means of the practical formula (El-Khayatt and Akkurt, 2013)

$$Z_{\text{eff}} = \frac{\sum_i f_i A_i \left(\frac{\mu}{\rho}\right)_i}{\sum_i f_i \frac{A_i}{Z_i} \left(\frac{\mu}{\rho}\right)_i} \quad (3)$$

The effective electron density, expressed in number of electrons per unit mass, is closely related to the effective atomic number and given by

$$N_{\text{eff}} = N_A \frac{Z_{\text{eff}}}{\langle A \rangle} \quad (4)$$

2.3 Half-value layer (HVL)

The half-value layer (HVL) is defined as the thickness of a shield or an absorber that reduces the radiation level by a factor of 2; that is, to half the initial level. (The HVL is also called a half-value thickness.) In this study, the HVL was calculated in units of (atom/cm²) using the atomic cross-section σ_a by the following equation:

$$x_{\frac{1}{2}} = HVL = \frac{0.693}{\sigma_a} \quad (5)$$

The mass attenuation coefficients for the elements at different photon energies were taken from Hubbell and Seltzer (1995). For comparisons, the shielding parameters for other types of concretes were calculated with the same method as for I-M concrete. The composition of barite, serpentine and ordinary concrete-1 was taken from Sharifi *et al.* (2013) and ordinary concrete-2 from Cember and Jonson (2009).

3 Results and discussions

3.1 Total atomic cross-section

The variation of the total atomic cross-section σ_a (barn/atom) of I-M concrete with photon energy is shown in Figure 1 and compared with concretes of different densities and compositions. In the low-energy range from a few keV to about 100 keV, the σ_a (barn/atom) for I-M concrete is higher than that of the ordinary concretes and serpentine. This is due to the higher values of mass attenuation coefficients of the elements of I-M concrete, which can be explained by the dominance of the photoelectric effect in this energy range. Since the photoelectric effect strongly depends on the atomic number of the element we can say that materials containing elements of higher atomic number will have a higher atomic cross-section. This is exactly what we can see from Figure 1. When the photon energy is exactly equal to the binding energy of the innermost K or L shell electron in the elements, σ_a (barn/atom) shows a peak in the curve known as the photoelectric edge. The sharp decrease in σ_a (barn/atom) is due to the energy dependence of the photoelectric effect.

In the intermediate energy region where Compton scattering is dominant, there is a smooth fall in the curve because this interaction depends inversely on photon energy. The σ_a (barn/atom) of I-M concrete is also found to be higher

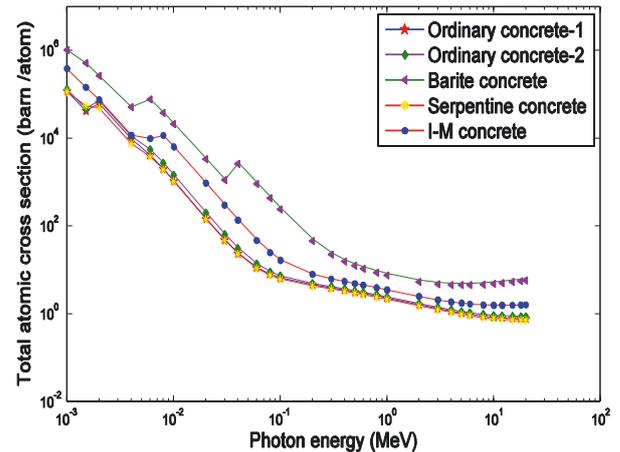


Figure 1. Variation of the total atomic cross-section with photon energy.

than that of the other concretes except barite, which contains 46.34% barium. Although serpentine has a higher effective electron density than I-M concrete, the elements of higher atomic masses in I-M concrete compensated for the effect of its lower electron density in this energy range. In the higher-energy region greater than 10 MeV, the probability of pair production increases with photon energy, which is shown by the smooth rise in the curve at the end. Also, in this region σ_a (barn/atom) of I-M concrete is higher than that of the serpentine and ordinary concretes. This can also be explained by the elements of higher atomic number in I-M concrete.

3.2 Total electronic cross-section (σ_e)

The total electronic cross-section σ_e (barn/electron) of any material at a particular energy depends mainly on the mass attenuation coefficient of the elements in the material at that particular energy. The ratio of atomic mass to atomic number does not have any significant effect on the electronic cross-section since it is nearly constant for all the elements in the periodic table except for the higher atomic number elements. However, the higher atomic number elements are favored by photoelectric absorption and pair production. The variation of σ_e (barn/electron) of different concretes with photon energy is shown in Figure 2. It is seen from the figure that σ_e (barn/electron) of I-M concrete is much higher than that of the ordinary concretes and serpentine in the low-energy region of up to 0.1 MeV where photoelectric absorption dominates the interaction process. This is because of the higher (μ/ρ) of the elements of I-M concrete. It is also seen from the figure that photoelectric absorption dominates over a greater energy range in the higher effective atomic number material than in the lower one. Peaks in the curve and the sharp decrease in σ_e (barn/electron) are also the consequences of photoelectric absorption. In the energy range from 0.5 MeV to 3 MeV, Compton scattering is dominant in all the materials and σ_e (barn/electron) is nearly the same for all materials irrespective of their effective atomic number. Moreover, the ratio A/Z is nearly constant for all the elements. Therefore, σ_e is the same for all materials at a particular energy. As energy increases beyond this region pair production starts to dominate,

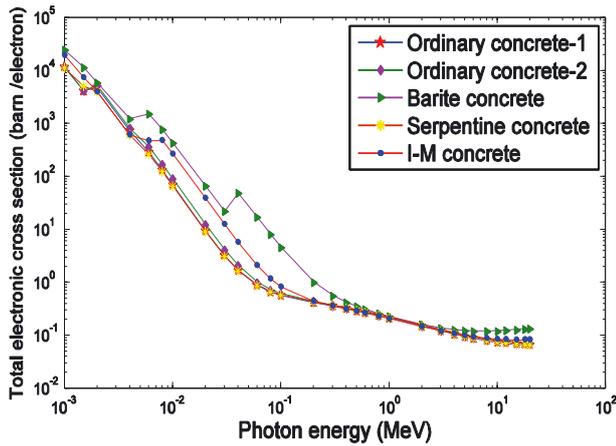


Figure 2. Variation of the total electronic cross-section with photon energy.

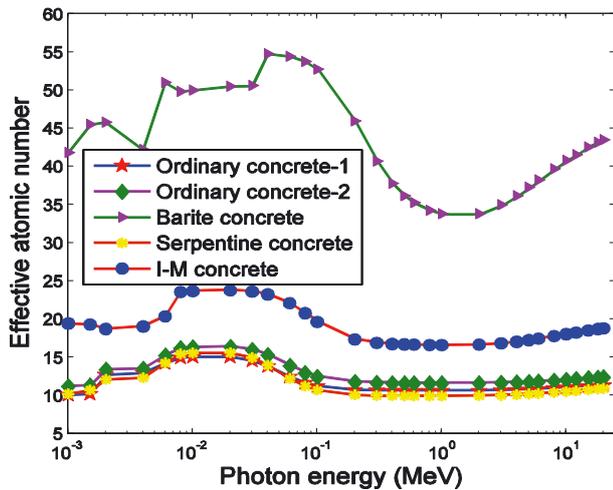


Figure 3. Variation of the effective atomic number with photon energy.

whose probability increases with both the photon energy and the effective atomic number of the material. Therefore, σ_e of the I-M concrete is higher than that of the other concretes except barite, which has the highest effective atomic number.

3.3 Effective atomic number (Z_{eff}) and effective electron density (N_{eff})

The effective atomic number of the I-M concrete at different photon energies is compared with other types of concretes in Figure 3. It is clear from the figure that I-M concrete has higher Z_{eff} values than the ordinary concretes and serpentine due to its higher atomic number elements. Barite, which contains nearly fifty percent barium, has the highest value of effective atomic number. The minimum Z_{eff} values were found in the intermediate region, where Compton scattering is dominant, which is independent of atomic number and approximately equal to the mean atomic number of the samples. The maximum value of Z_{eff} was found in the low-energy range, where photoelectric absorption is dominant. Figure 4 presents the variations of effective electron density (N_{eff}) of different

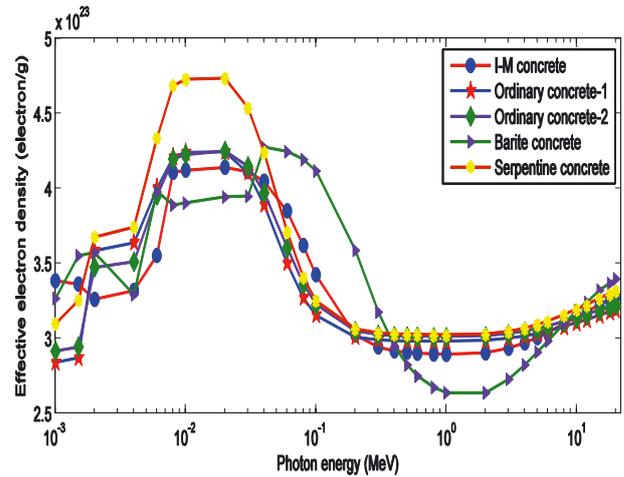


Figure 4. Variation of the effective electron density with photon energy.

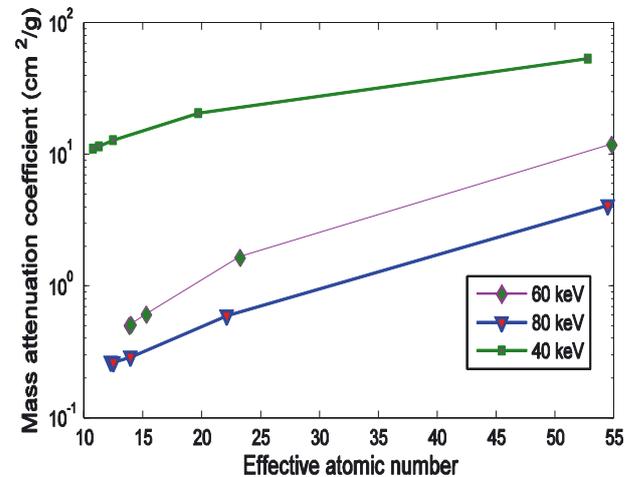


Figure 5. Variation of the mass attenuation coefficient with Z_{eff} .

concretes at photon energies from 1 keV to 20 MeV. Peaks in the curves indicate the photoelectric edge. Since incident photons interact with individual electrons, therefore higher N_{eff} means higher attenuation of photons. The effective electron density of I-M concrete is higher than that of the ordinary concretes and serpentine in the energy range where photoelectric absorption and pair production are dominant. In the intermediate energy region where Compton scattering is dominant, serpentine is slightly better than I-M concrete for its higher effective electron density. Figure 5 shows the variation of the total mass attenuation coefficient (μ/ρ) with Z_{eff} at low photon energies where photoelectric absorption is dominant. It is clear from Figure 5 that the μ/ρ at these energies strongly depends on Z_{eff} and increases with Z_{eff} . Figures 6 and 7 depict the dependence of the total electronic cross-section (σ_e) and total atomic cross-section (σ_a) on Z_{eff} , respectively. The variations observed were similar to those the case of μ/ρ . Therefore, the concretes with higher Z_{eff} will have higher σ_a and σ_e at these low energies where photoelectric absorption is dominant. Also, the higher the σ_a and σ_e , the better the shielding will be.

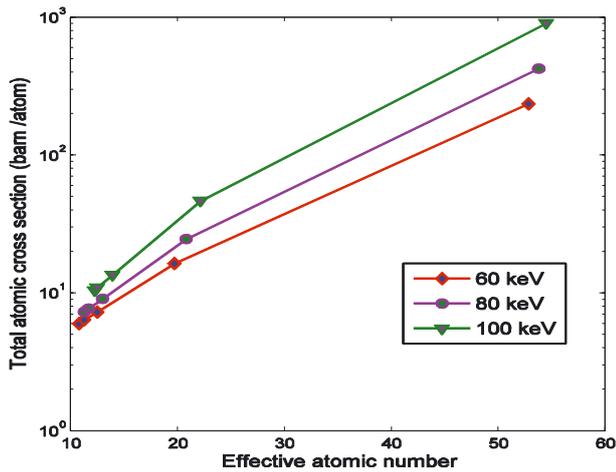


Figure 6. Variation of the total atomic cross-section with Z_{eff} .

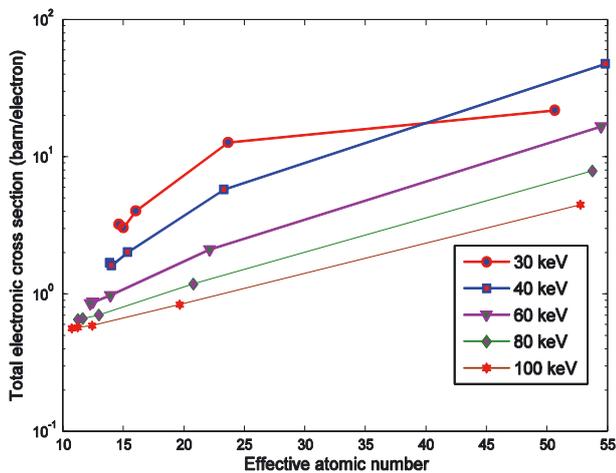


Figure 7. Variation of the total electronic cross-section with Z_{eff} .

4 Conclusions

The atomic cross-section, electronic cross-section, effective atomic number and effective electron density calculated in this study reflect the good quality of I-M concrete as far as its shielding properties are concerned. The effective electron density (N_{eff}) and effective atomic number (Z_{eff}) are closely related and they have the same qualitative energy dependence. The mass attenuation coefficient (μ/ρ) of the element is a useful and sensitive physical quantity to determine the (Z_{eff}) and (N_{eff}) of a concrete. The results of this study will provide a database for these parameters for this locally developed concrete as well as for other types of concretes, which will facilitate the shielding design problem. It can be concluded that I-M concrete is superior to ordinary concretes in the whole energy range and better than serpentine in the region where the photoelectric effect and pair production are dominant. Since raw materials are locally available, I-M concrete will be an excellent, cost-effective and less space-consuming shielding

material against gamma rays. It can be used as a shield for reactors, accelerators, X-ray installation and other hot laboratories, as well as commercial gamma-ray irradiation facilities.

References

- Ahmed F.U., Bhuiyan S.I., Mollah A.S., Rahman M.M. (1992) Measurement of gamma ray shielding properties of ilmenite-magnetite concrete and polyborn slabs using a ^{252}Cf source, *Nuclear Technology* **98**, 379-386.
- Ahmed F.U., Bhuiyan S.I., Mollah A.S., Sarder M.R., Huda M.Q., Rahman M., Mondal M.A.W. (1999) Studies on the shielding properties of polyboron and ilmenite-magnetite concrete using a reactor beam, *Nuclear Technology* **126**, 196-204.
- Al-Jaff S.M.A.A. (2013) Investigation the Effective atomic number, electron density, Half value layer and mean free path of steel types 304 and 347 in the energy range 40 KeV-130 KeV, *Journal of Natural Sciences Research* **3**, 15.
- Bhuiyan S.I., Ahmed F.U., Mollah A.S., Rahman M.A. (1991) Studies of neutron shielding properties of ilmenite- magnetite concrete using a ^{252}Cf source, *Nuclear Technology* **93**, 357-361.
- Cember H., Jonson E. (2009) *Introduction to Health Physics*, fourth ed. Chapt. 5, Department of Environmental and Radiological Health Sciences Colorado State University.
- El-Khayatt A.M., Akkurt I. (2013) Photon interaction, energy absorption and neutron removal cross section of concrete including marble, *Ann. Nucl. Energy* **60**, 814.
- Han I., Demir L. (2009) Mass attenuation coefficients, effective atomic and electron numbers of Ti and Ni alloys, *Radiat. Meas.* **44**, 289-294.
- Han I., and Demir L. (2010) Studies on the effective atomic number, electron densities and mass attenuation coefficients in Au alloys, *Journal of X-Ray Science and Technology* **18**, 39-46.
- Hubbell J.H., Seltzer S.M. (1995) Tables of X-ray Mass Attenuation Coefficients and Mass Energy-Absorption Coefficients 1 keV to 20 MeV for Elements $Z = 1$ to 92 and 48 Additional Substances of Dosimetric Interest. NISTIR-5632, National Institute of Standards and Technology, Gaithersburg.
- Kucuk N., Cakir M., Isitman N.A. (2013) Mass Attenuation Coefficients, Effective Atomic Numbers And Effective Electron Densities For Some Polymers, *Radiat. Prot. Dosim.* **153**, 127-134.
- Madhusudhan Rao A.S., Narender K., Gopal Kishan Rao K., Gopi Krishna N., Radha Krishna Murthy (2013) Mass Attenuation Coefficients, Effective atomic and Electron Numbers of Alkali Halides for Multi-Energetic Photons, *Research Journal of Physical Sciences* **1** (6), 11-16.
- Medhat M.E. (2011) Studies on effective atomic numbers and electron densities in different solid state track detectors in the energy range 1 keV-100 GeV, *Ann. Nucl. Energy* **38**, 1252-1263.
- Sharifi Sh., Bagheri R., Shirmardi S.P. (2013) Comparison of shielding properties for ordinary, barite, serpentine and steel magnetite concretes using MCNP-4C code and available experimental results, *Ann. Nucl. Energy* **53**, 529-534.
- Singh V.P., Badiger N.M. (2013) Study of mass attenuation coefficients, effective atomic numbers and electron densities of carbon steel and stainless steels, *Radioprotection* **48**, 431-443.
- Yılmaz E., Baltas H., Kırıs E., Ustabas I., Cevik U., El-Khayatt A.M. (2011) Gamma ray and neutron shielding properties of some concrete materials, *Ann. Nucl. Energy* **38**, 2204-2222.